IMAGING PROPERTIES OF LENS SYSTEMS

THE OPTICAL INVARIANT
To understand the importance of the NA, consider its relation to magnification. Referring to figure 4.6,

\[
\text{NA (object side)} = \sin \theta = \frac{CA}{2s} \quad (4.10)
\]

\[
\text{NA" (image side)} = \sin \theta" = \frac{CA}{2s"} \quad (4.11)
\]

which can be rearranged to show

\[
\frac{s"}{s} = \frac{\sin \theta}{\sin \theta"} = \frac{\text{NA}}{\text{NA"}} \quad (4.12)
\]

and

\[
\frac{1}{s} = 2s" \sin \theta \quad (4.13)
\]

leading to

\[
\frac{s"}{s} = \frac{\sin \theta}{\sin \theta"} = \frac{\text{NA}}{\text{NA"}} \quad (4.14)
\]

Since \( \frac{s"}{s} \) is simply the magnification of the system, we arrive at

\[
m = \frac{\text{NA}}{\text{NA"}} \quad (4.15)
\]

The magnification of the system is therefore equal to the ratio of the NAs on the object and image sides of the system. This powerful and useful result is completely independent of the specifics of the optical system, and it can often be used to determine the optimum lens diameter in situations involving aperture constraints.

When a lens or optical system is used to create an image of a source, it is natural to assume that, by increasing the diameter (\( \Phi \)) of the lens, thereby increasing its CA, we will be able to collect more light and thereby produce a brighter image. However, because of the relationship between magnification and NA, there can be a theoretical limit beyond which increasing the diameter has no effect on light-collection efficiency or image brightness.

Since the NA of a ray is given by CA/2s, once a focal length and magnification have been selected, the value of NA sets the value of CA. Thus, if one is dealing with a system in which the NA is constrained on either the object or image side, increasing the lens diameter beyond this value will increase system size and cost but will not improve performance (i.e., throughput or image brightness). This concept is sometimes referred to as the optical invariant.

SAMPLE CALCULATION
To understand how to use this relationship between magnification and NA, consider the following example.

EXAMPLE: SYSTEM WITH FIXED INPUT NA
Two very common applications of simple optics involve coupling light into an optical fiber or into the entrance slit of a monochromator. Although these problems appear to be quite different, they both have the same limitation – they have a fixed NA. For monochromators, this limit is usually expressed in terms of the f-number. In addition to the fixed NA, they both have a fixed entrance pupil (image) size.

Suppose it is necessary, using a singlet lens, to couple the output of an incandescent bulb with a filament 1 mm in diameter into an optical fiber as shown in figure 4.7. Assume that the fiber has a core diameter of 100 mm and an NA of 0.25, and that the design requires that the total distance from the source to the fiber be 110 mm. Which lenses are appropriate?

By definition, the magnification must be 0.1. Letting \( s + s" \) total 110 mm (using the thin-lens approximation), we can use equation 4.3,

\[
f = \frac{m (s + s")}{(m + 1)^2}, \quad \text{(see eq. 4.3)}
\]

to determine that the focal length is 9.1 mm. To determine the conjugate distances, \( s \) and \( s" \), we utilize
equation 4.6,

\[ s(m+1) = s + s'' \]

(see eq. 4.6)

and find that \( s = 100 \text{ mm} \) and \( s'' = 10 \text{ mm} \).

We can now use the relationship \( \text{NA} = \frac{CA}{2s} \) or \( \text{NA}'' = \frac{CA}{2s''} \) to derive \( CA \), the optimum clear aperture (effective diameter) of the lens.

With an image NA of 0.25 and an image distance \( (s'') \) of 10 mm,

\[ 0.25 = \frac{CA}{20} \]

\[ \text{CA} = 5 \text{ mm} \]

Accomplishing this imaging task with a single lens therefore requires an optic with a 9.1 mm focal length and a 5 mm diameter. Using a larger diameter lens will not result in any greater system throughput because of the limited input NA of the optical fiber. The singlet lenses in this catalog that meet these criteria are LPX-5.0-5.2-C, which is plano-convex, and LDX-6.0-7.7-C and LDX-5.0-9.9-C, which are biconvex.

Making some simple calculations has reduced our choice of lenses to just three. The following chapter, Gaussian Beam Optics, discusses how to make a final choice of lenses based on various performance criteria.