

MATERIAL PROPERTIES

INTRODUCTION	T-44
OPTICAL PROPERTIES	T-45
MECHANICAL AND CHEMICAL PROPERTIES	T-47
LENS MATERIALS	T-49
CALCIUM FLUORIDE.....	T-50
UV-GRADE SYNTHETIC FUSED SILICA.....	T-51
SUPRASIL 1	T-53
CRYSTAL QUARTZ.....	T-54
SCHOTT GLASS	T-56
CROWN GLASS.....	T-57
MATERIAL PROPERTIES OVERVIEW.....	T-58

INTRODUCTION

Glass manufacturers provide hundreds of different glass types with differing optical transmission and mechanical strengths. CVI Laser Optics has simplified the task of selecting the right material for an optical component by offering each of our standard components in a single material, or in a small range of materials best suited to typical applications.

There are, however, two instances in which one might need to know more about optical materials: one might need to determine the performance of a catalog component in a particular application, or one might need specific information to select a material for a custom component. The information given in this chapter is intended to assist in that process.

The most important material properties to consider in regard to an optical element are as follows:

- ▶ Transmission versus wavelength
- ▶ Index of refraction
- ▶ Thermal characteristics
- ▶ Mechanical characteristics
- ▶ Chemical characteristics
- ▶ Cost

TRANSMISSION VERSUS WAVELENGTH

A material must transmit efficiently at the wavelength of interest if it is to be used for a transmissive component. A transmission curve allows the optical designer to estimate the attenuation of light as a function of wavelength caused by internal material properties. For mirror substrates, the attenuation may be of no consequence.

INDEX OF REFRACTION

The index of refraction, as well as the rate of change of index with wavelength (dispersion), might require consideration. High-index materials allow the designer to achieve a given power with less surface curvature, typically resulting in lower aberrations. On the other hand, most high-index flint glasses have higher dispersion, resulting in more chromatic aberration in polychromatic applications. They also typically have poorer chemical characteristics than lower-index crown glasses.

THERMAL CHARACTERISTICS

The thermal expansion coefficient can be particularly important in applications in which the part is subjected to high temperatures, such as high-intensity projection systems. This is also of concern when components must undergo large temperature cycles, such as in optical systems used outdoors.

MECHANICAL CHARACTERISTICS

The mechanical characteristics of a material are significant in many areas. They can affect how easy it is to fabricate the material into shape, which affects product cost. Scratch resistance is important if the component will require frequent cleaning. Shock and vibration resistance are important for military, aerospace, or certain industrial applications. Ability to withstand high pressure differentials is important for windows used in vacuum chambers.

CHEMICAL CHARACTERISTICS

The chemical characteristics of a material, such as acid or stain resistance, can also affect fabrication and durability. As with mechanical characteristics, chemical characteristics should be taken into account for optics used outdoors or in harsh conditions.

COST

Cost is almost always a factor to consider when specifying materials. Furthermore, the cost of some materials, such as UV-grade synthetic fused silica, increases sharply with larger diameters because of the difficulty in obtaining large pieces of the material.

OPTICAL PROPERTIES

The most important optical properties of a material are its internal and external transmittances, surface reflectance, and refractive index. The formulas that connect these variables in the on-axis case are presented below.

TRANSMISSION

External transmittance is the single-pass irradiance transmittance of an optical element. Internal transmittance is the single-pass irradiance transmittance in the absence of any surface reflection losses (i.e., transmittance of the material itself). External transmittance is of paramount importance when selecting optics for an image-forming lens system because external transmittance neglects multiple reflections between lens surfaces. Transmittance measured with an integrating sphere will be slightly higher. If T_e denotes the desired external irradiance transmittance, T_i the corresponding internal transmittance, t_1 the single-pass transmittance of the first surface, and t_2 the single-pass transmittance of the second surface, then

$$T_e = t_1 t_2 T_i = t_1 t_2 e^{-\mu t_c} \quad (2.1)$$

where e is the base of the natural system of logarithms, μ is the absorption coefficient of the lens material, and t_c is the lens center thickness. This allows for the possibility that the lens surfaces might have unequal transmittances (for example, one is coated and the other is not). Assuming that both surfaces are uncoated,

$$t_1 t_2 = 1 - 2r + r^2 \quad (2.2)$$

where

$$r = \left(\frac{n-1}{n+1} \right)^2 \quad (2.3)$$

is the single-surface single-pass irradiance reflectance at normal incidence as given by the Fresnel formula. The refractive index n must be known or calculated from the material dispersion formula found in the next section.

These results are applicable to monochromatic. Both μ and n are functions of wavelength.

To calculate either T_i or the T_e for a lens at any wavelength of interest, first find the value of absorption coefficient μ . Typically, internal transmittance T_i is tabulated as a function of wavelength for two distinct thicknesses t_{c1} and t_{c2} , and m must be found from these.

Thus where the bar denotes averaging. In portions of the spectrum where absorption is strong, a value for T_i is typically given only for the lesser thickness. Then

$$\mu = -\frac{1}{t_c} \ln T_i \quad (2.5)$$

When it is necessary to find transmittance at wavelengths other than those for which T_i is tabulated, use linear interpolation.

The on-axis T_e value is normally the most useful, but some applications require that transmittance be known along other ray paths, or that it be averaged over the entire lens surface. The method outlined above is easily extended to encompass such cases. Values of t_1 and t_2 must be found from complete Fresnel formulas for arbitrary angles of incidence. The angles of incidence will be different at the two surfaces; therefore, t_1 and t_2 will generally be unequal. Distance t_c , which becomes the surface-to-surface distance along a particular ray, must be determined by ray tracing. It is necessary to account separately for the s - and p -planes of polarization, and it is usually sufficient to average results for both planes at the end of the calculation.

REFRACTIVE INDEX AND DISPERSION

The Schott Optical Glass catalog offers nearly 300 different optical glasses. For lens designers, the most important difference among these glasses is the index of refraction and dispersion (rate of change of index with wavelength). Typically, an optical glass is specified by its index of refraction at a wavelength in the middle of the visible spectrum, usually 587.56 nm (the helium d-line), and by the Abbé v -value, defined to be $v_d = (n_d - 1) / (n_F - n_C)$. The designations F and C stand for 486.1 nm and 656.3 nm, respectively. Here, v_d shows how the index of refraction varies with wavelength. The

smaller v_d is, the faster the rate of change is. Glasses are roughly divided into two categories: crowns and flints. Crown glasses are those with $n_d < 1.60$ and $v_d > 55$, or $n_d > 1.60$ and $v_d > 50$. The others are flint glasses.

The refractive index of glass from 365 to 2300 nm can be calculated by using the formula

$$n^2 - 1 = \frac{B_1\lambda^2}{\lambda^2 - C_1} + \frac{B_2\lambda^2}{\lambda^2 - C_2} + \frac{B_3\lambda^2}{\lambda^2 - C_3} \quad (2.6)$$

Here λ , the wavelength, must be in micrometers, and the constants B_1 through C_3 are given by the glass manufacturer. Values for other glasses can be obtained from the manufacturer's literature. This equation yields an index value that is accurate to better than 1×10^{-5} over the entire transmission range, and even better in the visible spectrum.

OTHER OPTICAL CHARACTERISTICS

REFRACTIVE INDEX HOMOGENEITY

The tolerance for the refractive index within melt for all Schott fine annealed glass used in CVI Laser Optics catalog components is $\pm 1 \times 10^{-4}$. Furthermore, the refractive index homogeneity, a measure of deviation within a single piece of glass, is better than $\pm 2 \times 10^{-5}$.

STRIAE GRADE

Striae are thread-like structures representing subtle but visible differences in refractive index within an optical glass. Striae classes are specified in ISO 10110. All CVI Laser Optics catalog components that utilize Schott optical glass are specified to have striae that conform to ISO 10110 class 5 indicating that no visible striae, streaks, or cords are present in the glass.

STRESS BIREFRINGENCE

Mechanical stress in optical glass leads to birefringence (anisotropy in index of refraction) which can impair the optical performance of a finished component. Optical glass is annealed (heated and cooled) to remove any residual stress left over from the original manufacturing process. Schott Glass defines fine annealed glass to have a stress birefringence of less than or equal to 10 nm/cm for diameters less than 300 mm and for thicknesses less than or equal to 60 mm. For diameters between 300 and 600 mm and for thicknesses between 60 and 80 mm, stress birefringence would be less than or equal to 12 nm/cm.

APPLICATION NOTE

Fused-Silica Optics

Synthetic fused silica is an ideal optical material for many laser applications. It is transparent from as low as 180 nm to over 2.0 μm , has low coefficient of thermal expansion, and is resistant to scratching and thermal shock.

MECHANICAL AND CHEMICAL PROPERTIES

Mechanical and chemical properties of glass are important to lens manufacturers. These properties can also be significant to the user, especially when the component will be used in a harsh environment. Different polishing techniques and special handling may be needed depending on whether the glass is hard or soft, or whether it is extremely sensitive to acid or alkali.

To quantify the chemical properties of glasses, glass manufacturers rate each glass according to four categories: climatic resistance, stain resistance, acid resistance, and alkali and phosphate resistance.

CLIMATIC RESISTANCE

Humidity can cause a cloudy film to appear on the surface of some optical glass. Climatic resistance expresses the susceptibility of a glass to high humidity and high temperatures. In this test, glass is placed in a water vapor-saturated environment and subjected to a temperature cycle which alternately causes condensation and evaporation. The glass is given a rating from 1 to 4 depending on the amount of surface scattering induced by the test. A rating of 1 indicates little or no change after 30 hours of climatic change; a rating of 4 means a significant change occurred in less than 30 hours.

STAIN RESISTANCE

Stain resistance expresses resistance to mildly acidic water solutions, such as fingerprints or perspiration. In this test, a few drops of a mild acid are placed on the glass. A colored stain, caused by interference, will appear if the glass starts to decompose. A rating from 0 to 5 is given to each glass, depending on how much time elapses before stains occur. A rating of 0 indicates no observed stain in 100 hours of exposure; a rating of 5 means that staining occurred in less than 0.2 hours.

ACID RESISTANCE

Acid resistance quantifies the resistance of a glass to stronger acidic solutions. Acid resistance can be particularly important to lens manufacturers because acidic solutions are typically used to strip coatings from glass or to separate cemented elements. A rating from 1 to 4 indicates progressively less resistance to a pH 0.3 acid solution, and values from 51 to 53 are used for glass with too little resistance to be tested with such a strong solution.

ALKALI AND PHOSPHATE RESISTANCE

Alkali resistance is also important to the lens manufacturer since the polishing process usually takes place in an alkaline solution. Phosphate resistance is becoming more significant as users move away from cleaning methods that involve chlorofluorocarbons (CFCs) to those that may be based on traditional phosphate-containing detergents. In each case, a two-digit number is used to designate alkali or phosphate resistance. The first number, from 1 to 4, indicates the length of time that elapses before any surface change occurs in the glass, and the second digit reveals the extent of the change.

MICROHARDNESS

The most important mechanical property of glass is microhardness. A precisely specified diamond scribe is placed on the glass surface under a known force. The indentation is then measured. The Knoop and the Vickers microhardness tests are used to measure the hardness of a polished surface and a freshly fractured surface, respectively.

Knoop Hardness Values for Standard Optical Materials

Material	Knoop Hardness
Magnesium Fluoride	415
Calcium Fluoride	158
Fused Silica	522
BK7 (N-BK7)	610
Optical Crown Glass	542
Borosilicate Glass	480
Zerodur	620
Zinc Selenide	112
Silicon	1100
Germanium	780

APPLICATION NOTE

Glass Manufacturers

The catalogs of optical glass manufacturers contain products covering a very wide range of optical characteristics. However, it should be kept in mind that the glass types that exhibit the most desirable properties in terms of index of refraction and dispersion often have the least practical chemical and mechanical characteristics. Furthermore, poor chemical and mechanical attributes translate directly into increased component costs because working these sensitive materials increases fabrication time and lowers yield. Please contact us before specifying an exotic glass in an optical design so that we can advise you of the impact that that choice will have on part fabrication.

LENS MATERIALS

CVI Laser Optics lenses are made of synthetic fused silica, N-BK7 grade A fine annealed glass, and several other materials. The following table identifies the materials used in CVI Laser Optics lenses. Some of these materials are also used in prisms, mirror substrates, and other products.

Glass type designations and physical constants are the same as those published by Schott Glass. CVI Laser Optics occasionally uses corresponding glasses made by other glass manufacturers but only when this does not result in a significant change in optical properties.

The performance of optical lenses and prisms depends on the quality of the material used. No amount of skill during manufacture can eradicate striae, bubbles, inclusions, or variations in index. CVI Laser Optics takes considerable care in its material selection, using only first-class optical materials from reputable glass manufacturers. The result is reliable, repeatable, consistent performance.

The following physical constant values are reasonable averages based on historical experience. Individual material specimens may deviate from these means. Materials having tolerances more restrictive than those published in the rest of this chapter, or materials traceable to specific manufacturers, are available only on special request.

N-BK7 OPTICAL GLASS

A borosilicate crown glass, N-BK7, is the material used in many CVI Laser Optics products. N-BK7 performs well in chemical tests so that special treatment during polishing is not necessary. N-BK7, a relatively hard glass, does not scratch easily and can be handled without special precautions. The bubble and inclusion content of N-BK7 is very low, with a cross-section total less than 0.029 mm² per 100 cm³. Another important characteristic of N-BK7 is its excellent transmittance, at wavelengths as low as 350 nm. Because of these properties, N-BK7 is used widely throughout the optics industry. A variant of N-BK7, designated UBK7, has transmission at wavelengths as low as 300 nm. This special glass is useful in applications requiring a high index of refraction, the desirable chemical properties of N-BK7, and transmission deeper

into the ultraviolet range. N-BK7 refers to the lead and arsenic-free version of BK7, with most optical properties identical between the two.

CVI Laser Optics reserves the right, without prior notice, to make material changes or substitution on any optical component.

Lens Material Table

Material	Product Code	
Synthetic Fused Silica UV Grade	LUP-UV	LUK-UV
	PLCX-UV	PLCC-UV
	BICX-UV	BICC-UV
	RCX-UV	RCC-UV
	SCX-UV	SCC-UV
	CLCX-UV	CLCC-UV
	BFPL-UV	
N-BK7 Grade A Fine Annealed	LPX-C	LPK-C
	PLCX-C	PLCC-C
	LDX-C	
	BICX-C	BICC-C
	SCX-C	SCC-C
SK11 and SF5 Grade A Fine Annealed	LAI	
SF11 Grade-A Fine Annealed	PLCX-SF11	PLCC-SF11
Optical Crown Glass	LAG	
Calcium Fluoride	PLCX-CFUV	
Magnesium Fluoride		
Various Glass Combinations (including lead- and arsenic-free glasses)	LAO	LAL

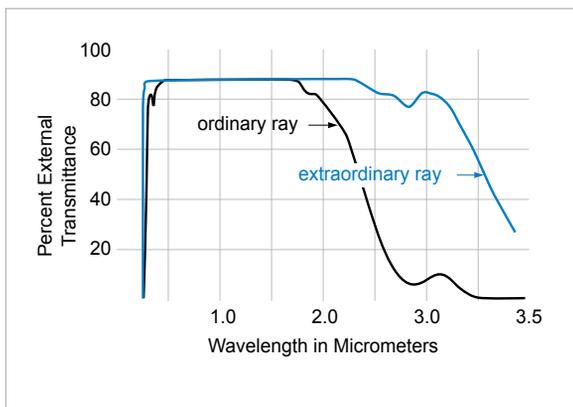
CALCIUM FLUORIDE

Calcium fluoride (CaF_2), a cubic single-crystal material, has widespread applications in the ultraviolet and infrared spectrum. CaF_2 is an ideal material for use with excimer lasers. It can be manufactured into windows, lenses, prisms, and mirror substrates.

CaF_2 transmits over the spectral range of about 130 nm to 10 μm . Traditionally, it has been used primarily in the infrared, rather than in the ultraviolet. CaF_2 occurs naturally and can be mined. It is also produced synthetically using the time- and energy-consuming Stockbarger method. Unfortunately, achieving acceptable deep ultraviolet transmission and damage resistance in CaF_2 requires much greater material purity than in the infrared, and it completely eliminates the possibility of using mined material.

To meet the need for improved component lifetime and transmission at 193 nm and below, manufacturers have introduced a variety of inspection and processing methods to identify and remove various impurities at all stages of the production process. The needs for improved material homogeneity and stress birefringence have also caused producers to make alterations to the traditional Stockbarger approach. These changes allow tighter temperature control during crystal growth, as well as better regulation of vacuum and annealing process parameters.

Excimer-grade CaF_2 provides the combination of deep ultraviolet transmission (down to 157 nm), high damage threshold, resistance to color-center formation, low fluorescence, high homogeneity, and low stress-birefringence characteristics required for the most demanding deep ultraviolet applications.



External transmittance for 5 mm thick uncoated calcium fluoride

Specifications

Density: 3.18 g/cm³ @ 25°C

Young's Modulus: 1.75x10⁷ psi

Poisson's Ratio: 0.26

Knoop Hardness: 158

Thermal Coefficient of Refraction: $dn/dT = -10.6 \times 10^{-6}/^\circ\text{C}$

Coefficient of Thermal Expansion: $18.9 \times 10^{-6}/^\circ\text{C}$ (20°–60°C)

Melting Point: 1360°C

Dispersion Constants:

B1 = 0.5675888

B2 = 0.4710914

B3 = 3.8484723

C1 = 0.00252643

C2 = 0.01007833

C3 = 1200.5560

Refractive Index of Calcium Fluoride

Wavelength (μm)	Index of Refraction
0.193	1.501
0.248	1.468
0.257	1.465
0.266	1.462
0.308	1.453
0.355	1.446
0.486	1.437
0.587	1.433
0.65	1.432
0.7	1.431
1.0	1.428
1.5	1.426
2.0	1.423
2.5	1.421
3.0	1.417
4.0	1.409
5.0	1.398
6.0	1.385
7.0	1.369
8.0	1.349

UV-GRADE SYNTHETIC FUSED SILICA

Synthetic fused silica (amorphous silicon dioxide), by chemical combination of silicon and oxygen, is an ideal optical material for many applications. It is transparent over a wide spectral range, has a low coefficient of thermal expansion, and is resistant to scratching and thermal shock.

The synthetic fused silica materials used by CVI Laser Optics are manufactured by flame hydrolysis to extremely high standards. The resultant material is colorless and non-crystalline, and it has an impurity content of only about one part per million.

Synthetic fused silica lenses offer a number of advantages over glass or fused quartz:

- ▶ Greater ultraviolet and infrared transmission
- ▶ Low coefficient of thermal expansion, which provides stability and resistance to thermal shock over large temperature excursions
- ▶ Wider thermal operating range
- ▶ Increased hardness and resistance to scratching
- ▶ Much higher resistance to radiation darkening from ultraviolet, x-rays, gamma rays, and neutrons.

UV-grade synthetic fused silica (UVGSFS or Suprasil 1) is selected to provide the highest transmission (especially in the deep ultraviolet) and very low fluorescence levels (approximately 0.1% that of fused natural quartz excited at 254 nm). UV-grade synthetic fused silica does not fluoresce in response to wavelengths longer than 290 nm. In deep ultraviolet applications, UV-grade synthetic fused silica is an ideal choice. Its tight index tolerance ensures highly predictable lens specifications.

The batch-to-batch internal transmittance of synthetic fused silica may fluctuate significantly in the near infrared between 900 nm and 2.5 μm due to resonance absorption by OH chemical bonds. If the optic is to be used in this region, Infrasil 302 may be a better choice.

Specifications

Abbé Constant: 67.8 ± 0.5

Change of Refractive Index with Temperature (0° to 700°C): $1.28 \times 10^{-5}/^\circ\text{C}$

Homogeneity (maximum index variation over 10-cm aperture): 2×10^{-5}

Density: 2.20 g/cm^3 @ 25°C

Knoop Hardness: 522

Continuous Operating Temperature: 900°C maximum

Coefficient of Thermal Expansion: $5.5 \times 10^{-7}/^\circ\text{C}$

Specific Heat: $0.177 \text{ cal/g}^\circ\text{C}$ @ 25°C

Dispersion Constants:

$B_1 = 0.6961663$

$B_2 = 0.4079426$

$B_3 = 0.8974794$

$C_1 = 0.0046791$

$C_2 = 0.0135121$

$C_3 = 97.9340025$

Refractive Index of UV-Grade Synthetic Fused Silica*

Wavelength (nm)	Index of Refraction
180.0	1.58529
190.0	1.56572
200.0	1.55051
213.9	1.53431
226.7	1.52275
230.2	1.52008
239.9	1.51337
248.3	1.50840
265.2	1.50003
275.3	1.49591
280.3	1.49404
289.4	1.49099
296.7	1.48873
302.2	1.48719
330.3	1.48054
340.4	1.47858
351.1	1.47671
361.1	1.47513
365.0	1.47454
404.7	1.46962
435.8	1.46669

* Accuracy $\pm 3 \times 10^{-5}$

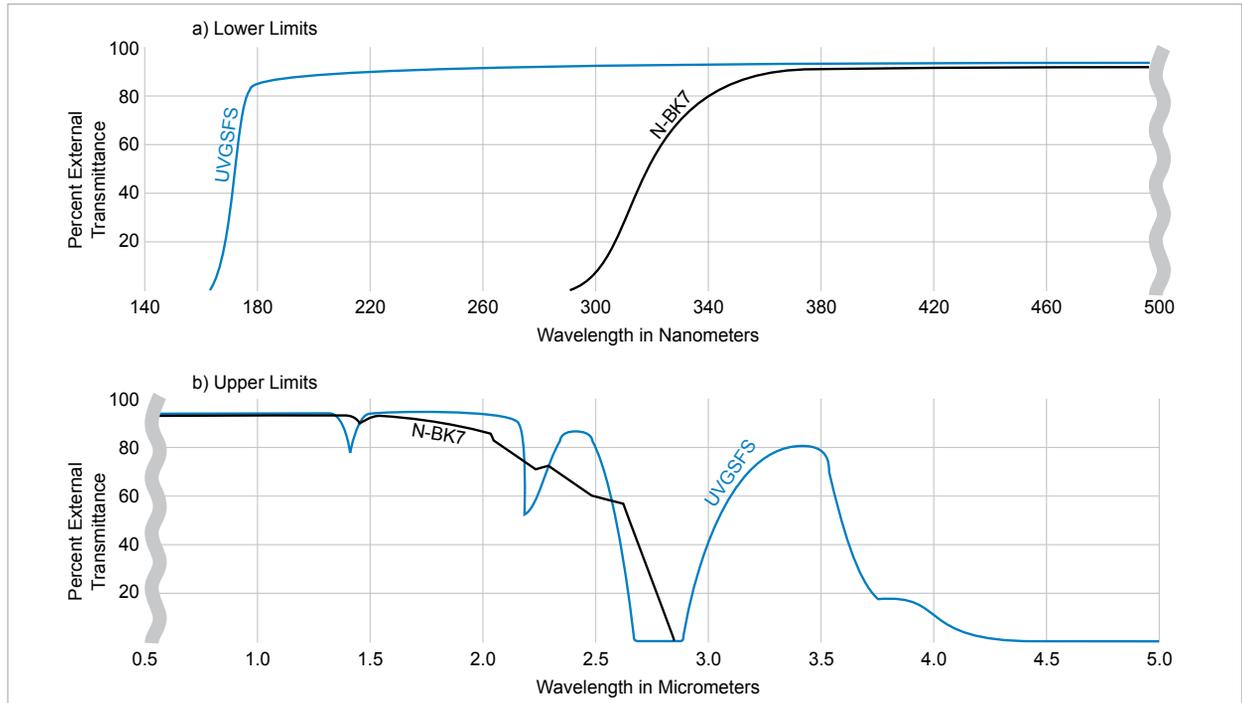
Refractive Index of UV-Grade Synthetic Fused Silica*

Wavelength (nm)	Index of Refraction
441.6	1.46622
457.9	1.46498
476.5	1.46372
486.1	1.46313
488.0	1.46301
496.5	1.46252
514.5	1.46156
532.0	1.46071
546.1	1.46008
587.6	1.45846
589.3	1.45840
632.8	1.45702
643.8	1.45670
656.3	1.45637
694.3	1.45542
706.5	1.45515
786.0	1.45356
820.0	1.45298

Refractive Index of UV-Grade Synthetic Fused Silica*

Wavelength (nm)	Index of Refraction
830.0	1.45282
852.1	1.45247
904.0	1.45170
1014.0	1.45024
1064.0	1.44963
1100.0	1.44920
1200.0	1.44805
1300.0	1.44692
1400.0	1.44578
1500.0	1.44462
1550.0	1.44402
1660.0	1.44267
1700.0	1.44217
1800.0	1.44087
1900.0	1.43951
2000.0	1.43809
2100.0	1.43659

* Accuracy $\pm 3 \times 10^{-5}$



Comparison of uncoated external transmittances for UVGSFS and N-BK7, all 10 mm in thickness

SUPRASIL 1

Suprasil 1 is a type of fused silica with high chemical purity and excellent multiple axis homogeneity. With a metallic content less than 8 ppm, Suprasil 1 has superior UV transmission and minimal fluorescence. Suprasil 1 is primarily used for low fluorescence UV windows, lenses and prisms where multiple axis homogeneity is required.

Specifications

Abbé Constant: 67.8 ± 0.5

Change of Refractive Index with Temperature (0° to 700°C):
 $1.28 \times 10^{-5}/^\circ\text{C}$

Homogeneity (maximum index variation over 10-cm aperture):
 2×10^{-5}

Knoop Hardness: 590

Density: 2.20 g/cm^3 @ 25°C

Continuous Operating Temperature: 900°C maximum

Coefficient of Thermal Expansion: $5.5 \times 10^{-7}/^\circ\text{C}$

Specific Heat: $0.177 \text{ cal/g}^\circ\text{C}$ @ 25°C

Dispersion Constants:

$B_1 = 0.6961663$

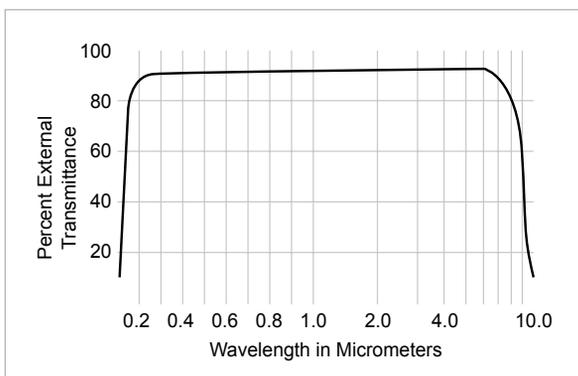
$B_2 = 0.4079426$

$B_3 = 0.8974794$

$C_1 = 0.0046791$

$C_2 = 0.0135121$

$C_3 = 97.9340025$



External transmittance for 5 mm thick uncoated calcium fluoride

Refractive Index of Suprasil 1*

Wavelength (nm)	Index of Refraction
193.4	1.56013
248.4	1.50833
266.0	1.49968
308.0	1.48564
325.0	1.48164
337.0	1.47921
365.5	1.47447
404.7	1.46962
435.8	1.46669
441.6	1.46622
447.1	1.46578
486.1	1.46313
488.0	1.46301
514.5	1.46156
532.0	1.46071
546.1	1.46008
587.6	1.45846
632.8	1.45702
656.3	1.45637
694.3	1.45542
752.5	1.45419
905.0	1.45168
1064.0	1.44963
1153.0	1.44859
1319.0	1.44670

* Accuracy $\pm 3 \times 10^{-5}$

CRYSTAL QUARTZ

Crystal quartz is a positive uniaxial birefringent single crystal grown using a hydrothermal process. Crystal quartz from CVI Laser Optics is selected to minimize inclusions and refractive index variation. Crystal quartz is most commonly used for high-damage-threshold waveplates and solarization-resistant Brewster windows for argon lasers.

The dispersion for the index of refraction is given by the Laurent series shown below.

$$\eta^2 = A_0 + A_1\lambda^2 + \frac{A_2}{\lambda^2} + \frac{A_3}{\lambda^4} + \frac{A_4}{\lambda^6} + \frac{A_5}{\lambda^8}$$

Specifications

Transmission Range: 0.170–2.8 μm

Melting Point: 1463°C

Knoop Hardness: 741

Density: 2.64 g/cm³

Young's Modulus, Perpendicular: 76.5 GPa

Young's Modulus, Parallel: 97.2 GPa

Thermal Expansion Coefficient, Perpendicular: 13.2x10⁻⁶/°C

Thermal Expansion Coefficient, Parallel: 7.1x10⁻⁶/°C

Dispersion Constants (Ordinary Ray):

A₀=2.35728

A₁=41.17000x10⁻²

A₂=1.05400x10⁻²

A₃=1.34143x10⁻⁴

A₄=44.45368x10⁻⁷

A₅=5.92362x10⁻⁸

Dispersion Constants (Extraordinary Ray):

A₀=2.38490

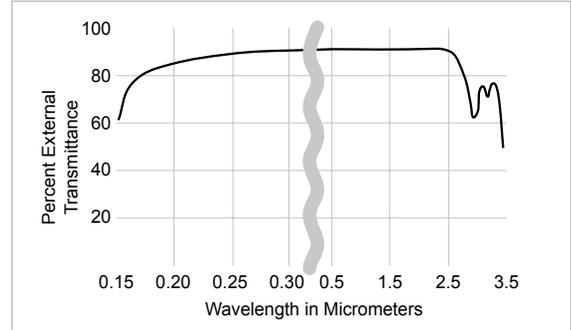
A₁=41.25900x10⁻²

A₂=1.07900x10⁻²

A₃=1.65180x10⁻⁴

A₄=41.94741x10⁻⁷

A₅=9.36476x10⁻⁸



External transmittance for 10 mm thick uncoated crystal quartz

Refractive Index of Crystal Quartz

Wavelength (nm)	Index of Refraction Ordinary Ray (n _o)	Index of Refraction Extraordinary Ray (n _e)
193	1.66091	1.67455
213	1.63224	1.64452
222	1.62238	1.63427
226	1.61859	1.63033
244	1.60439	1.61562
248	1.60175	1.61289
257	1.59620	1.60714
266	1.59164	1.60242
280	1.58533	1.59589
308	1.57556	1.58577
325	1.57097	1.58102
337	1.56817	1.57812
351	1.56533	1.57518
355	1.56463	1.57446
400	1.55772	1.56730
442	1.55324	1.56266
458	1.55181	1.56119
488	1.54955	1.55885
515	1.54787	1.55711
532	1.54690	1.55610
590	1.54421	1.55333
633	1.54264	1.55171
670	1.54148	1.55051
694	1.54080	1.54981
755	1.53932	1.54827
780	1.53878	1.54771
800	1.53837	1.54729
820	1.53798	1.54688
860	1.53724	1.54612
980	1.53531	1.54409

SCHOTT GLASS

The following tables list the most important optical and physical constants for Schott optical glass types BK7, SF11, LaSFN9, BaK1, and F2, with N-BK7 and N-BaK1 denoting the lead and arsenic-free versions of BK7 and BaK1. These types are used in most CVI Laser Optics simple lens products and prisms. Index of refraction as well as the most commonly required chemical characteristics and mechanical constants, are listed. Further numerical data and a more detailed discussion of the various testing processes can be found in the Schott Optical Glass catalog.

Physical Constants of Schott Glasses

	Glass Type				
	BK7 (N-BK7)	SF11	LaSFN9	BaK1 (N-BaK1)	F2
Melt-to-Melt Mean Index Tolerance	±0.0005	±0.0005	±0.0005	±0.0005	±0.0005
Stress Birefringence nm/cm Yellow Light	10	10	10	10	10
Abbé Factor (v_d)	64.17	25.76	32.17	57.55	36.37
Constants of Dispersion Formula:					
B_1	1.03961212	1.73848403	1.97888194	1.12365662	1.34533359
B_2	$2.31792344 \times 10^{-1}$	$3.11168974 \times 10^{-1}$	$3.20435298 \times 10^{-1}$	$3.09276848 \times 10^{-1}$	$2.09073176 \times 10^{-1}$
B_3	1.01046945	1.17490871	1.92900751	$8.81511957 \times 10^{-1}$	$9.37357162 \times 10^{-1}$
C_1	$6.00069867 \times 10^{-3}$	$1.36068604 \times 10^{-4}$	$1.18537266 \times 10^{-2}$	$6.44742752 \times 10^{-3}$	$9.97743871 \times 10^{-3}$
C_2	$2.00179144 \times 10^{-2}$	$6.15960463 \times 10^{-2}$	$5.27381770 \times 10^{-2}$	$2.22284402 \times 10^{-2}$	$4.70450767 \times 10^{-2}$
C_3	$1.03560653 \times 10^{-2}$	$1.21922711 \times 10^{-2}$	$1.66256540 \times 10^{-2}$	$1.07297751 \times 10^{-2}$	$1.11886764 \times 10^{-2}$
Density (g/cm ³)	2.51	4.74	4.44	3.19	3.61
Coefficient of Linear Thermal Expansion (cm/°C):					
-30° to +70°C	7.1×10^{-6}	6.1×10^{-6}	7.4×10^{-6}	7.6×10^{-6}	8.2×10^{-6}
+20° to +300°C	8.3×10^{-6}	6.8×10^{-6}	8.4×10^{-6}	8.6×10^{-6}	9.2×10^{-6}
Transition Temperature	557°C	505°C	703°C	592°C	438°C
Young's Modulus (dynes/mm ²)	8.20×10^9	6.60×10^9	1.09×10^{10}	7.30×10^9	5.70×10^9
Climate Resistance	2	1	2	2	1
Stain Resistance	0	0	0	1	0
Acid Resistance	1.0	1.0	2.0	3.3	1.0
Alkali Resistance	2.0	1.2	1.0	1.2	2.3
Phosphate Resistance	2.3	1.0	1.0	2.0	1.3
Knoop Hardness	610	450	630	530	420
Poisson's Ratio	0.206	0.235	0.286	0.252	0.220

SCHOTT GLASS

Refractive Index of various Schott Glass

Wavelength λ (nm)	Refractive Index, n					Fraunhofer Designation	Source	Spectral Region
	BK7 (N-BK7)	SF11	LaSFN9	BaK1 (N-BaK1)	F2			
351.1	1.53894	—	—	1.60062	1.67359		Ar laser	UV
363.8	1.53649	—	—	1.59744	1.66682		Ar laser	UV
404.7	1.53024	1.84208	1.89844	1.58941	1.65064	h	Hg arc	Violet
435.8	1.52668	1.82518	1.88467	1.58488	1.64202	g	Hg arc	Blue
441.6	1.52611	1.82259	1.88253	1.58415	1.64067		HeCd laser	Blue
457.9	1.52461	1.81596	1.87700	1.58226	1.63718		Ar laser	Blue
465.8	1.52395	1.81307	1.87458	1.58141	1.63564		Ar laser	Blue
472.7	1.52339	1.81070	1.87259	1.58071	1.63437		Ar laser	Blue
476.5	1.52309	1.80946	1.87153	1.58034	1.63370		Ar laser	Blue
480.0	1.52283	1.80834	1.87059	1.58000	1.63310	F'	Cd arc	Blue
486.1	1.52238	1.80645	1.86899	1.57943	1.63208	F	H ₂ arc	Blue
488.0	1.52224	1.80590	1.86852	1.57927	1.63178		Ar laser	Blue
496.5	1.52165	1.80347	1.86645	1.57852	1.63046		Ar laser	Green
501.7	1.52130	1.80205	1.86524	1.57809	1.62969		Ar laser	Green
514.5	1.52049	1.79880	1.86245	1.57707	1.62790		Ar laser	Green
532.0	1.51947	1.79479	1.85901	1.57580	1.62569		Nd laser	Green
546.1	1.51872	1.79190	1.85651	1.57487	1.62408	e	Hg arc	Green
587.6	1.51680	1.78472	1.85025	1.57250	1.62004	d	He arc	Yellow
589.3	1.51673	1.78446	1.85002	1.57241	1.61989	D	Na arc	Yellow
632.8	1.51509	1.77862	1.84489	1.57041	1.61656		HeNe laser	Red
643.8	1.51472	1.77734	1.84376	1.56997	1.61582	C'	Cd arc	Red
656.3	1.51432	1.77599	1.84256	1.56949	1.61503	C	H ₂ arc	Red
694.3	1.51322	1.77231	1.83928	1.56816	1.61288		Ruby laser	Red
786.0	1.51106	1.76558	1.83323	1.56564	1.60889			IR
821.0	1.51037	1.76359	1.83142	1.56485	1.60768			IR
830.0	1.51020	1.76311	1.83098	1.56466	1.60739		GaAlAs	laser IR
852.1	1.50980	1.76200	1.82997	1.56421	1.60671	s	Ce arc	IR
904.0	1.50893	1.75970	1.82785	1.56325	1.60528		GaAs laser	IR
1014.0	1.50731	1.75579	1.82420	1.56152	1.60279	t	Hg arc	IR
1060.0	1.50669	1.75445	1.82293	1.56088	1.60190		Nd laser	IR
1300.0	1.50370	1.74901	1.81764	1.55796	1.59813		InGaAsP laser	IR
1500.0	1.50127	1.74554	1.81412	1.55575	1.59550			IR
1550.0	1.50065	1.74474	1.81329	1.55520	1.59487			IR
1970.1	1.49495	1.73843	1.80657	1.55032	1.58958		Hg arc	IR
2325.4	1.48921	1.73294	1.80055	1.54556	1.58465		Hg arc	IR

CROWN GLASS

In optical crown glass, a low-index commercial-grade glass, the index of refraction, transmittance, and homogeneity are not controlled as carefully as they are in optical-grade glasses such as N-BK7. Optical crown glass is suitable for applications in which component tolerances are fairly loose, and as a substrate material for mirrors.

Specifications

Glass Type Designation: B270

Abbé Constant: 58.5

Dispersion: $(n_F - n_C) = 0.0089$

Knoop Hardness: 542

Density: 2.55 g/cm³ @ 23°C

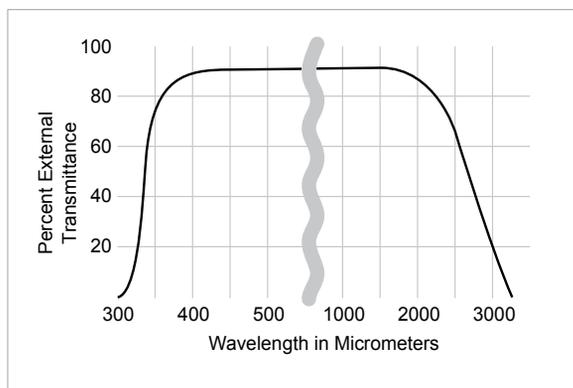
Young's Modulus: 71.5 kN/mm²

Specific Heat: 0.184 cal/g/°C (20°C to 100°C)

Coefficient of Thermal Expansion: $93.3 \times 10^{-7}/^{\circ}\text{C}$ (20°C to 300°C)

Transformation Temperature: 521°C

Softening Point: 708°C



External transmittance for 10 mm thick uncoated optical crown glass

Refractive Index of Optical Crown Glass

Wavelength (nm)	Index of Refraction	Fraunhofer Designation	Source	Spectral Region
435.8	1.53394	g	Hg arc	Blue
480.0	1.52960	F'	Cd arc	Blue
486.1	1.52908	F	H ₂ arc	Blue
546.1	1.52501	e	Hg arc	Green
587.6	1.52288	d	He arc	Yellow
589.0	1.52280	D	Na arc	Yellow
643.8	1.52059	C'	Cd arc	Red
656.3	1.52015	C	H ₂ arc	Red

Transmission Values for 6 mm thick Sample

Wavelength (nm)	Transmission (%)
300.0	0.3
310.0	7.5
320.0	30.7
330.0	56.6
340.0	73.6
350.0	83.1
360.0	87.2
380.0	88.8
400.0	90.6
450.0	90.9
500.0	91.4
600.0	91.5

MATERIAL PROPERTIES OVERVIEW

